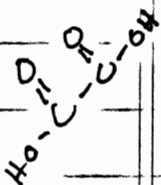
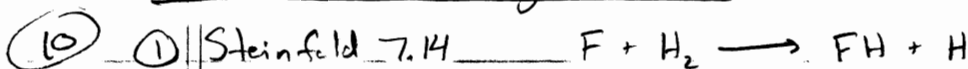


34 pts.

CHM5250 - Assignment #3



$D_{FH} = 591.1 \text{ kJ/mol}$

$D_{HH} = 458.2 \text{ kJ/mol}$

$\beta_{FH} = 2.2189 \text{ \AA}^{-1}$

$\beta_{HH} = 1.9420 \text{ \AA}^{-1}$

$r_{FH}^0 = 0.917 \text{ \AA}$

$r_{HH}^0 = 0.7419 \text{ \AA}$

$S_{FH} = 0.167$

$S_{HH} = 0.106$

$$V(r_{FH_1}, r_{H_1H_2}, r_{FH_2}) = \frac{Q_{FH_1}}{1+S_{FH_1}} + \frac{Q_{1-2}}{1+S_{1-2}} + \frac{Q_{F-2}}{1+S_{F-2}} - \left\{ \frac{1}{2} \left[\left(\frac{J_{F-1}}{1+S_{F-1}} - \frac{J_{1-2}}{1+S_{1-2}} \right)^2 + \left(\frac{J_{1-2}}{1+S_{1-2}} - \frac{J_{F-2}}{1+S_{F-2}} \right)^2 + \left(\frac{J_{F-2}}{1+S_{F-2}} - \frac{J_{F-1}}{1+S_{F-1}} \right)^2 \right] \right\}^{1/2}$$

F-H₁ and F-H₂ will both use the FH set of parameters - it is still an F atom and an H atom.

$r_{F-H_2} = r_{F-H_1} + r_{H_1H_2} = r_{FH} + r_{HH}$

$Q_{FH_1} + J_{FH_1} = D_{FH_1} \left\{ \exp[-2\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] - 2 \exp[-\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] \right\}$

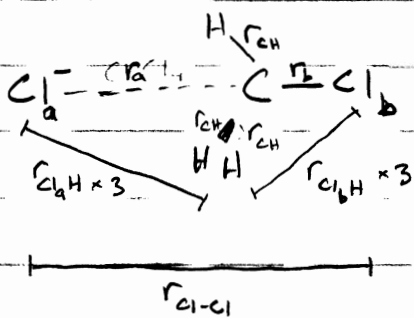
$Q_{FH_1} - J_{FH_1} = \frac{1}{2} D_{FH_1} \left\{ \exp[-2\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] + 2 \exp[-\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] \right\}$

Set this up in Excel!

$Q_{FH_1} = \left[(Q_{FH_1} + J_{FH_1}) + (Q_{FH_1} - J_{FH_1}) \right]^{1/2}$
 $= \frac{1}{2} \left[D_{FH_1} \left\{ \exp[-2\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] - 2 \exp[-\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] \right\} + \frac{1}{2} D_{FH_1} \times \left\{ \exp[-2\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] + 2 \exp[-\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] \right\} \right]$

$J_{FH_1} = \frac{1}{2} \left[(Q_{FH_1} + J_{FH_1}) - (Q_{FH_1} - J_{FH_1}) \right]$
 $= \frac{1}{2} \left[D_{FH_1} \left\{ \exp[-2\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] - 2 \exp[-\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] \right\} - \frac{1}{2} D_{FH_1} \times \left\{ \exp[-2\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] + 2 \exp[-\beta_{FH_1}(r_{FH_1} - r_{FH_1}^0)] \right\} \right]$

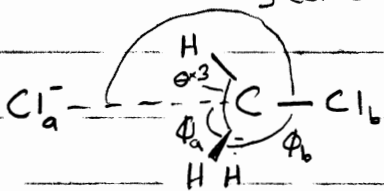
④ ② a. $\text{Cl}^- + \text{CH}_3\text{Cl}$



$$g_a = r_a - r_b$$

$$g_b = r_b - r_a$$

ξ (Cl-C-Cl angle)



③ b. $g_a + g_b$ give the difference in C-Cl distances - they measure the extent of reaction. If $g_a = g_b = 0$, then $r_a = r_b + r_{\text{ran}}$ is at the transition state. If $g_a > 0$ ($+ g_b < 0$), $r_a > r_b$ and Cl_a^- has not yet collided w/ the CH_3Cl . If $g_a < 0$ ($+ g_b > 0$), $r_a < r_b$ and Cl_a^- has already collided w/ the CH_3Cl so that the $\text{Cl}-\text{Cl}_b^-$ distance is now increasing.

⑥ c. # coord. = $3N - 6 = 3(6) - 6 = \boxed{12}$

In table 1, eight coords. are defined (less than the minimum), but there are actually three Cl-H distances for each Cl (6 total), three Cl-C-H angles for each Cl (6 total), ^{three C-H distances} and three H-C-H angles. This gives a total of:

- C-Cl_a
- C-Cl_b
- Cl_a-Cl_b
- Cl-H × 6
- C-H × 3
- Cl-C-H × 6
- H-C-H × 3
- Cl-C-Cl

It makes sense that many of these are redundant since, for instance, if three Cl-C-H angles and three C-H dist. are defined, then the H-C-H distances are determined by the other parameters → they are geometrically not independent. ^{it can be calc'd by trigonometry}

22 coords. → So there are ten redundant coords. plus $g_a + g_b$ (so really 12 red. coord.)

② Assignment #3 (cont.)

② c. (second c.) Short + long range discussed in paragraph after eqn (2):

② and d.

long range: $V_{LR}^a + V_{LR}^b$ terms (last two terms before $D_{MC} + D_c$)

short range: V_{Cl} terms (first two terms)

V_q terms (third + fourth terms)

V_{ClCl} term (fifth term)

V_θ term (sixth term)

V_{HC} term (seventh term)

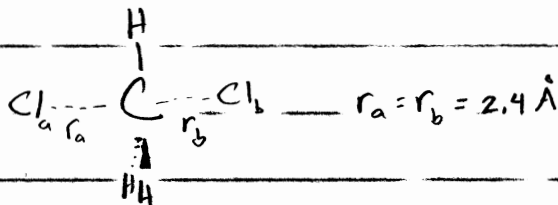
D_{MC}, D_c (bond energies \rightarrow short range)

Morse and/or
harmonic potential
functions

④ e. In the S_N2 reaction described in the paper, there are never any unpaired electrons. The Cl^- ion and CH_3Cl are both closed-shell species. This differs from $H_2 \rightarrow 2H$ in which the reactant is closed shell but the product is open shell. It is the change in pairing of electrons that HF calculations do not deal well with.

③ f. TS is the maximum on the contour plot in Fig. 7. This is at the point where $Cl_a-C = Cl_b-C$ ($r_a = r_b$). From the plot, this is a distance of $\sim 2.4 \text{ \AA}$.

Structure:



QFH1	RFH1	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6	
RH1H2	0.5	2075.506	60.89219	-47.7121	-23.1034	-8.41954	-2.8634	-0.95365	-0.31549	-0.10414	-0.03435	-0.01133	-0.00374
	1	2075.506	60.89219	-47.7121	-23.1034	-8.41954	-2.8634	-0.95365	-0.31549	-0.10414	-0.03435	-0.01133	-0.00374
	1.5	2075.506	60.89219	-47.7121	-23.1034	-8.41954	-2.8634	-0.95365	-0.31549	-0.10414	-0.03435	-0.01133	-0.00374
	2	2075.506	60.89219	-47.7121	-23.1034	-8.41954	-2.8634	-0.95365	-0.31549	-0.10414	-0.03435	-0.01133	-0.00374
	2.5	2075.506	60.89219	-47.7121	-23.1034	-8.41954	-2.8634	-0.95365	-0.31549	-0.10414	-0.03435	-0.01133	-0.00374
	3	2075.506	60.89219	-47.7121	-23.1034	-8.41954	-2.8634	-0.95365	-0.31549	-0.10414	-0.03435	-0.01133	-0.00374
	3.5	2075.506	60.89219	-47.7121	-23.1034	-8.41954	-2.8634	-0.95365	-0.31549	-0.10414	-0.03435	-0.01133	-0.00374
	4	2075.506	60.89219	-47.7121	-23.1034	-8.41954	-2.8634	-0.95365	-0.31549	-0.10414	-0.03435	-0.01133	-0.00374
	4.5	2075.506	60.89219	-47.7121	-23.1034	-8.41954	-2.8634	-0.95365	-0.31549	-0.10414	-0.03435	-0.01133	-0.00374
	5	2075.506	60.89219	-47.7121	-23.1034	-8.41954	-2.8634	-0.95365	-0.31549	-0.10414	-0.03435	-0.01133	-0.00374

QFH1	RFH1	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
RH1H2	0.5	512.8584	512.8584	512.8584	512.8584	512.8584	512.8584	512.8584	512.8584	512.8584	512.8584	512.8584
	1	-12.6742	-12.6742	-12.6742	-12.6742	-12.6742	-12.6742	-12.6742	-12.6742	-12.6742	-12.6742	-12.6742
	1.5	-34.4721	-34.4721	-34.4721	-34.4721	-34.4721	-34.4721	-34.4721	-34.4721	-34.4721	-34.4721	-34.4721
	2	-17.3103	-17.3103	-17.3103	-17.3103	-17.3103	-17.3103	-17.3103	-17.3103	-17.3103	-17.3103	-17.3103
	2.5	-7.16578	-7.16578	-7.16578	-7.16578	-7.16578	-7.16578	-7.16578	-7.16578	-7.16578	-7.16578	-7.16578
	3	-2.80124	-2.80124	-2.80124	-2.80124	-2.80124	-2.80124	-2.80124	-2.80124	-2.80124	-2.80124	-2.80124
	3.5	-1.07339	-1.07339	-1.07339	-1.07339	-1.07339	-1.07339	-1.07339	-1.07339	-1.07339	-1.07339	-1.07339
	4	-0.4083	-0.4083	-0.4083	-0.4083	-0.4083	-0.4083	-0.4083	-0.4083	-0.4083	-0.4083	-0.4083
	4.5	-0.15488	-0.15488	-0.15488	-0.15488	-0.15488	-0.15488	-0.15488	-0.15488	-0.15488	-0.15488	-0.15488
	5	-0.05869	-0.05869	-0.05869	-0.05869	-0.05869	-0.05869	-0.05869	-0.05869	-0.05869	-0.05869	-0.05869

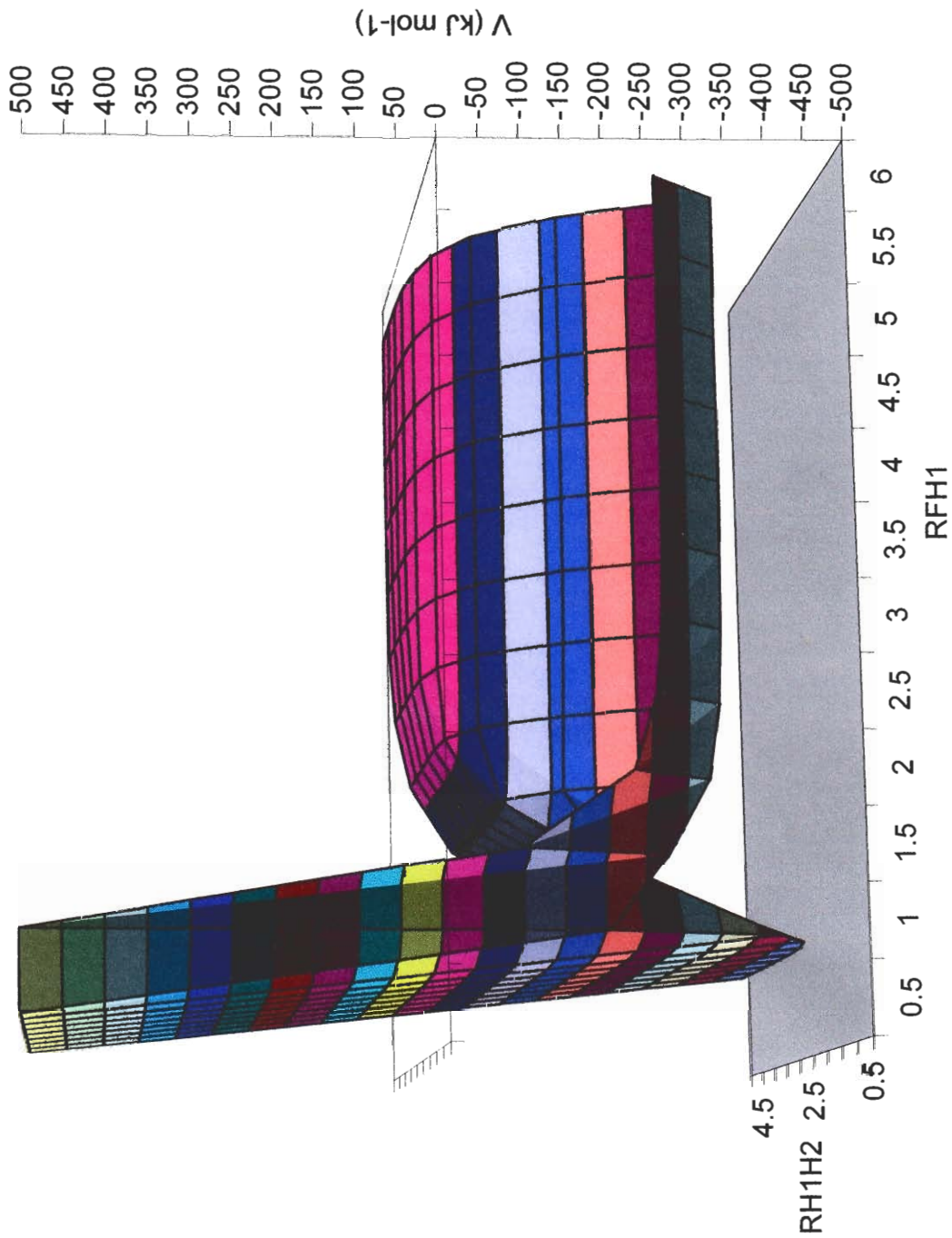
QFH2	RFH2	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6	
RH1H2	0.5	6978.093	476.8809	-41.0826	-35.1107	-13.922	-4.84559	-1.6255	-0.53901	-0.17806	-0.05875	-0.01938	-0.00639
	1	476.8809	-41.0826	-35.1107	-13.922	-4.84559	-1.6255	-0.53901	-0.17806	-0.05875	-0.01938	-0.00639	-0.00211
	1.5	-41.0826	-35.1107	-13.922	-4.84559	-1.6255	-0.53901	-0.17806	-0.05875	-0.01938	-0.00639	-0.00211	-0.00069
	2	-35.1107	-13.922	-4.84559	-1.6255	-0.53901	-0.17806	-0.05875	-0.01938	-0.00639	-0.00211	-0.00069	-0.00023
	2.5	-13.922	-4.84559	-1.6255	-0.53901	-0.17806	-0.05875	-0.01938	-0.00639	-0.00211	-0.00069	-0.00023	-7.6E-05
	3	-4.84559	-1.6255	-0.53901	-0.17806	-0.05875	-0.01938	-0.00639	-0.00211	-0.00069	-0.00023	-7.6E-05	-2.5E-05
	3.5	-1.6255	-0.53901	-0.17806	-0.05875	-0.01938	-0.00639	-0.00211	-0.00069	-0.00023	-7.6E-05	-2.5E-05	-8.2E-06
	4	-0.53901	-0.17806	-0.05875	-0.01938	-0.00639	-0.00211	-0.00069	-0.00023	-7.6E-05	-2.5E-05	-8.2E-06	-2.7E-06
	4.5	-0.17806	-0.05875	-0.01938	-0.00639	-0.00211	-0.00069	-0.00023	-7.6E-05	-2.5E-05	-8.2E-06	-2.7E-06	-8.9E-07
	5	-0.05875	-0.01938	-0.00639	-0.00211	-0.00069	-0.00023	-7.6E-05	-2.5E-05	-8.2E-06	-2.7E-06	-8.9E-07	-2.9E-07

Q+J(FH2)	RFH1	0.5	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
RH1H2		0.5	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
0.5	5903 547	-485 466	-424 517	-168 732	-58 7641	-19 7168	-6 53838	-2 15998	-0 71267	-0 23504	-0 07751	-0 02556	-0 00843
1	485 466	-424 517	-168 732	-58 7641	-19 7168	-6 53838	-2 15998	-0 71267	-0 23504	-0 07751	-0 02556	-0 00843	-0 000278
1.5	424 517	-168 732	-58 7641	-19 7168	-6 53838	-2 15998	-0 71267	-0 23504	-0 07751	-0 02556	-0 00843	-0 000278	-0 00092
2	-168 732	-58 7641	-19 7168	-6 53838	-2 15998	-0 71267	-0 23504	-0 07751	-0 02556	-0 00843	-0 000278	-0 00092	-0 0003
2.5	-58 7641	-19 7168	-6 53838	-2 15998	-0 71267	-0 23504	-0 07751	-0 02556	-0 00843	-0 000278	-0 00092	-0 0003	-1E-04
3	-19 7168	-6 53838	-2 15998	-0 71267	-0 23504	-0 07751	-0 02556	-0 00843	-0 000278	-0 00092	-0 0003	-1E-04	-3 3E-05
3.5	-6 53838	-2 15998	-0 71267	-0 23504	-0 07751	-0 02556	-0 00843	-0 000278	-0 00092	-0 0003	-1E-04	-3 3E-05	-1 1E-05
4	-2 15998	-0 71267	-0 23504	-0 07751	-0 02556	-0 00843	-0 000278	-0 00092	-0 0003	-1E-04	-3 3E-05	-1 1E-05	-3 6E-06
4.5	-0 71267	-0 23504	-0 07751	-0 02556	-0 00843	-0 000278	-0 00092	-0 0003	-1E-04	-3 3E-05	-1 1E-05	-3 6E-06	-1 2E-06
5	-0 23504	-0 07751	-0 02556	-0 00843	-0 000278	-0 00092	-0 0003	-0 0003	-1E-04	-3 3E-05	-1 1E-05	-3 6E-06	-1 2E-06

Q-J(FH2)	RFH1	0.5	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
RH1H2		0.5	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
0.5	8052 639	1439 228	342 3518	98 5111	30 91999	10 02561	3 287369	1 081969	0 35655	0 117545	0 038757	0 012779	0 004214
1	1439 228	342 3518	98 5111	30 91999	10 02561	3 287369	1 081969	0 35655	0 117545	0 038757	0 012779	0 004214	0 001389
1.5	342 3518	98 5111	30 91999	10 02561	3 287369	1 081969	0 35655	0 117545	0 038757	0 012779	0 004214	0 001389	0 000458
2	98 5111	30 91999	10 02561	3 287369	1 081969	0 35655	0 117545	0 038757	0 012779	0 004214	0 001389	0 000458	0 000151
2.5	30 91999	10 02561	3 287369	1 081969	0 35655	0 117545	0 038757	0 012779	0 004214	0 001389	0 000458	0 000151	4 98E-05
3	10 02561	3 287369	1 081969	0 35655	0 117545	0 038757	0 012779	0 004214	0 001389	0 000458	0 000151	4 98E-05	1 64E-05
3.5	3 287369	1 081969	0 35655	0 117545	0 038757	0 012779	0 004214	0 001389	0 000458	0 000151	4 98E-05	1 64E-05	5 42E-06
4	1 081969	0 35655	0 117545	0 038757	0 012779	0 004214	0 001389	0 000458	0 000151	4 98E-05	1 64E-05	5 42E-06	1 79E-06
4.5	0 35655	0 117545	0 038757	0 012779	0 004214	0 001389	0 000458	0 000151	4 98E-05	1 64E-05	5 42E-06	1 79E-06	5 89E-07
5	0 117545	0 038757	0 012779	0 004214	0 001389	0 000458	0 000151	4 98E-05	1 64E-05	1 64E-05	5 42E-06	1 79E-06	5 89E-07

V	RFH1	0.5	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
R _{H1H2} /R _{RFH1}		0.5	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
0.5	7891 105	677 7464	-91 07	-225 411	-254 124	-261 848	-264 204	-265 208	-264 961	-265 208	-265 289	-265 316	-265 324
1	1499 368	-205 514	-278 327	-329 701	-343 739	-347 928	-349 258	-349 834	-349 691	-349 834	-349 88	-349 896	-349 901
1.5	818 6544	-428 088	-224 146	-163 069	-164 526	-166 877	-167 802	-168 228	-168 122	-168 228	-168 264	-168 275	-168 279
2	704 4521	-474 111	-230 234	-94 4537	-68 4552	-67 8785	-68 4585	-68 812	-68 7191	-68 812	-68 8434	-68 8539	-68 8573
2.5	678 5637	-486 315	-235 867	-85 8759	-34 9148	-26 6821	-26 5048	-26 7686	-26 6864	-26 7686	-26 7981	-26 808	-26 8113
3	671 248	-490 148	-238 259	-86 3787	-29 5267	-12 5497	-10 1801	-10 2182	-10 1563	-10 2182	-10 2453	-10 2549	-10 2581
3.5	668 9124	-491 456	-239 186	-86 9991	-29 4041	-9 92539	-4 51052	-3 86531	-3 86027	-3 86531	-3 88678	-3 89577	-3 89893
4	668 125	-491 92	-239 536	-87 2871	-29 5914	-9 79171	-3 32121	-1 46174	-1 63434	-1 46174	-1 46732	-1 47475	-1 47774
4.5	667 8532	-492 086	-239 667	-87 403	-29 6915	-9 85108	-3 23825	-0 59792	-1 11379	-0 59792	-0 5535	-0 55646	-0 55902
5	667 7582	-492 147	-239 716	-87 4477	-29 7332	-9 88714	-3 25677	-0 37563	-1 06881	-0 37563	-0 22069	-0 20965	-0 21094

PES for F+H2 - Steinfeld Problem 7.14



PES for F+H2 - Steinfield Problem 7.14

